



**Operational Equations of State.
1. A Novel Equation of State for Hydrocode**

by M. A. Grinfeld

ARL-TR-5744

September 2011

NOTICES

Disclaimers

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy this report when it is no longer needed. Do not return it to the originator.

Army Research Laboratory

Aberdeen Proving Ground, MD 21005-5066

ARL-TR-5744**September 2011**

Operational Equations of State.

1. A Novel Equation of State for Hydrocode

M. A. Grinfeld

Weapons and Materials Research Directorate, ARL

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188		
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YYYY) September 2011		2. REPORT TYPE Final		3. DATES COVERED (From - To) 1 January 2011–8 January 2011	
4. TITLE AND SUBTITLE Operational Equations of State. 1. A Novel Equation of State for Hydrocode		5a. CONTRACT NUMBER			
		5b. GRANT NUMBER			
		5c. PROGRAM ELEMENT NUMBER			
6. AUTHOR(S) M. A. Grinfeld		5d. PROJECT NUMBER FPDT14A			
		5e. TASK NUMBER			
		5f. WORK UNIT NUMBER			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory ATTN: RDRL-WMP-B Aberdeen Proving Ground, MD 21005-5066		8. PERFORMING ORGANIZATION REPORT NUMBER ARL-TR-5744			
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S)			
		11. SPONSOR/MONITOR'S REPORT NUMBER(S)			
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT A novel model equation of state (EOS) for hydrocode is suggested. This model is called the $\Delta\chi$ -EOS because it depends on two functions of one variable each. The $\Delta\chi$ -EOS generalizes the classical incomplete EOS like the ideal gas thermal EOS, the van der Waals EOS, and the virial EOS, among others. We demonstrate the incomplete and complete variants of the $\Delta\chi$ -EOS. We also discuss how to recover the functions Δ and χ from experimental measurements.					
15. SUBJECT TERMS Mie-Grüneisen, EOS, shock waves, thermodynamics					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON
a. REPORT UNCLASSIFIED	b. ABSTRACT UNCLASSIFIED	c. THIS PAGE UNCLASSIFIED	UU	18	M. A. Grinfeld
					19b. TELEPHONE NUMBER (Include area code) (410) 278-7030

Contents

Acknowledgments	iv
1. Introduction	1
2. The Suggested Model	2
2.1 Recovery of the Functions $\chi(E)$ and $\Delta(V)$ From Measurements	4
2.1.1 The Hugoniot Adiabata Data.....	4
2.1.2 The Quasistatic Adiabata Data	4
2.2 Verification of Equations 1 and 2 for the EOS (5).....	5
3. Discussion and Conclusion	6
4. References	7
Distribution List	8

Acknowledgments

The author is grateful to Drs. Becker, Bilyk, Mennikov, and Segletes for useful discussions.

1. Introduction

The equation of state (EOS) is one of the most important notions in thermodynamics. A vast variety of the EOS has been suggested during several centuries of developing thermodynamics. Various applications in dealing with high pressure can be found in references 1 and 2. During those centuries, the very concept of the EOS itself was significantly changed, modified, and specialized by the greatest minds of physics, engineering, and mathematics. Because thermodynamics is a main interest for various disciplines and communities, different meanings are often assigned to the same terms. In the monograph in reference 3, the author discusses this semi-linguistic Babel Tower phenomenon regarding the term “chemical potential.” Not surprisingly, no full terminological consensus exists between the authors of the valuable reviews (4–8). Therefore, in order to avoid possible misinterpretation, we briefly describe our own interpretation of the existing terminology regarding the EOS.

The notion of the EOS appeared well before the discovery of the First Law of Thermodynamics. At that time, the EOS was the function linking pressure P , volume V , and empirical temperature τ – $P = P(V, \tau)$ of a gas or liquid. Today, many researchers call this a thermal EOS.

The discovery of the First Law of Thermodynamics introduced the concept of the internal energy E . This was treated as a function of the volume and empirical temperature $E = E(V, \tau)$ and often called the caloric EOS. Functions $P(V, \tau)$ and $E(V, \tau)$ are deeply connected with each other and cannot be assigned independently of each other. Otherwise, the First Law of Thermodynamics will be violated. Taken separately, none of the functions $P(V, \tau)$ and $E(V, \tau)$ are sufficient for describing all thermodynamic properties of substances.

Later, the discovery and acceptance of the Second Law of Thermodynamics entailed introduction of the absolute temperature T and entropy S . This law reveals an even deeper connection between the functions of thermal and caloric EOS than the First Law did. Moreover, the Second Law suggests treating the internal energy not as the function of the variables (V, τ) but as the function of the pair (V, S) : $E = E(V, S)$. The most meticulous theorists call this the complete EOS (see Menikoff [8]). Here, “complete” emphasizes that this function taken alone contains as much information as the two functions $P(V, \tau)$ and $E(V, \tau)$ together. At last, when the complete EOS in the form $E = E(V, S)$ is resolved with respect to the entropy, we arrive at the following EOS: $S = S(V, E)$. The last one is coined as the complete EOS for hydrocode. In this very sense, the term complete EOS for hydrocode is used in this report.

The logical foundations of classical thermodynamics remain under much criticism—this is a natural process emphasizing the importance of thermodynamics. Fortunately, this rarely leads to

revising the key universal identities valid for complete EOS. Practitioners rarely experience dissatisfaction with the canonical identities for the EOS. However, a variety of novel EOS for novel substances is needed. Because of the technological and engineering advances, even for traditional substances, practitioners demand the extension of the earlier accepted EOS for considerably wider domains of the parameter space. Also, there is an opposite demand of developing various simplified EOS suited for a specific engineering situation.

From a physics and applied mathematics standpoint, the EOS appear to be simple and conceptually transparent in two polar cases. First, the simplicity is achieved in the “big picture” approach of the classical thermodynamics when the most important features only are explicitly taken into account, whereas the variety of minor features deliberately remain unspecified. Second, the simplicity appears in the opposite case of extremely specialized models (e.g., the perfect gas model). Besides being useful in understanding physical phenomena, these cases also allow deep theoretical analysis.

It is now universally accepted that no single EOS can work for all purposes, all substances, and all ranges of thermodynamic parameters. Even if such a universal model were developed, it would only be useful for blind computer implementations and not for further theoretical analysis or intuitive comprehension. Theoretical analysis, however, is very important, even in the computer era.

We suggest a novel model that is rather simple and conceptually transparent. It possesses some features of the big and small pictures previously mentioned. It has infinitely many parametric degrees of freedom. However, the infinitely many degrees of freedom appear not in the form of infinitely many unrelated parameters but in the form of two *functional* degrees of freedom. This model is complete in the thermodynamic sense and includes some classical models as special cases. At the same time, it appears to be convenient for converting the shock-wave locus or the static adiabata locus into the EOS. Explicit formulas of this conversion are given next.

We call our models operational EOS's. The term operational is used because of two reasons. First, the suggested EOS's mostly have the form of various operators with respect to the experimental data used in their definitions. Second, they have direct relation to the Bridgman methodology of operationalism. We will discuss these methodological issues in forthcoming reports after demonstrating several important examples.

2. The Suggested Model

The suggested model is not as general as the most general models of classical thermodynamics. In fact, we suggest a class of the EOS for the hydrocode based on the following two simple constraints:

1. The heat capacity at constant volume C_V is a function of the internal energy density E only:

$$C_V = \chi(E). \quad (1)$$

2. The nondimensional combination PV / RT is a function of the volume V only:

$$\frac{PV}{RT} = \Delta(V), \quad (2)$$

where R is the universal thermodynamic constant.

Some classical EOS's are automatically included in this category. For instance, the model of the monoatomic perfect gas belongs to this category with the following choice of the parametric functions:

$$\chi(E) = \frac{3R}{2}, \quad \Delta(V) = 1. \quad (3)$$

Another example is the monoatomic van der Waals gas with the vanishing correction coefficient for the internal gas pressure. This classical model corresponds to the following choice of the functions:

$$\chi(E) = \frac{3}{2}R, \quad \Delta(V) = \frac{V}{V-b}. \quad (4)$$

In view of what was discussed in the Introduction, even the most innocent-looking assumptions can be thermodynamically inconsistent. In other words, there may not exist any complete EOS for which those assumptions can be deduced in a thermodynamically consistent way. It can be demonstrated, however, that the assumptions 1 and 2 are thermodynamically consistent for any of the two meaningful functions $\chi(E)$ and $\Delta(V)$. Moreover, such a potential can be presented in the following explicit form:

$$S(V, E) - S^* = \int_{V^*}^V d\varpi \frac{R\Delta(\varpi)}{\varpi} + \int_{E_*}^E \frac{d\xi}{H(\xi)}; \quad H(\xi) \equiv A + \int_{E_*}^{\xi} \frac{d\eta}{\chi(\eta)}, \quad (5)$$

where A is a constant. The function H has the physical meaning of the absolute temperature.

A simple verification of thermodynamic consistency and validity of equations 1, 2, and 5 is presented in section 2.2.

For the gas model described by equation 4, the EOS implies the following complete EOS for hydrocode:

$$S(V, E) = R \ln \frac{V - b}{V^* - b} + \frac{3R}{2} C_v \ln \frac{E - E_* + C_v A}{C_v A}. \quad (6)$$

2.1 Recovery of the Functions $\chi(E)$ and $\Delta(V)$ From Measurements

The class of substances described by the $\Delta\chi$ -EOS is much wider than the classical models. In fact, this class contains two arbitrary functions which can be specified based on the available sets of experimental data.

2.1.1 The Hugoniot Adiabata Data

Given the Hugoniot adiabat locus $E_H(V)$, we get the following Rankine-Hugoniot relationship (8–10):

$$2E_H(V) + P(V, E_H(V))(V - V_*) - 2E_* + P_*(V - V_*) = 0, \quad (7)$$

which implies the following formula of $\Delta(V)$:

$$\Delta(V) = \frac{2E_H(V) - 2E_* - P_*(V_* - V)}{RH(E_H(V))} \frac{V}{V_* - V} \quad (8)$$

and the following complete EOS for hydrocode:

$$S(V, E) = S^* + \int_{E^*}^E d\varepsilon \frac{1}{H(\varepsilon)} + \int_{V^*}^V d\varpi \frac{2E_H(\varpi) - 2E_* - P_*(V_* - \varpi)}{(V_* - \varpi)H(E_H(\varpi))}. \quad (9)$$

In the case of vanishing ambient pressure $P_* = 0$ and when the heat capacity C_v is constant, we arrive at the following simple EOS:

$$S(V, E) = S^* + C_v \ln \frac{E - E_* + C_v T^*}{C_v T^*} + \int_{V^*}^V d\varpi \frac{2E_H(\varpi) - 2E_*}{(V_* - \varpi)[E_H(\varpi) - E_* + C_v T^*]}, \quad (10)$$

where T^* is the ambient temperature.

Equations 9 and 10 show that inversion of the experimental measurements of the heat capacity $C_v(E)$ and the Hugoniot locus $E_H(V)$ into the complete EOS for hydrocode $S(V, E)$ is fulfilled with the help of the integral operator. The operator has singularity in the vicinity of the ambient configuration.

2.1.2 The Quasistatic Adiabata Data

The kernel of the integral operator in the recovery formula has a singularity near the ambient state, i.e., for the weak shock waves. Therefore, in the vicinity of the ambient state, some other approaches to recovering the EOS should be used.

The quasistatic adiabata is given by equation $E = E_s^*(V)$. Using equation 5, we get the following inversion:

$$S(V, E) = \int_{E_s^*(V)}^E d\xi \frac{1}{T^* + \int_{E_*}^{\xi} \frac{d\eta}{\chi(\eta)}} + S^*. \quad (11)$$

In the case of constant heat capacity at fixed volume, equation 11 reads as follows:

$$S(V, E) - S^* = C_v \ln \frac{E - E_* + C_v T^*}{E_s^*(V) - E_* + C_v T^*}. \quad (12)$$

Equations 11 and 12 show that inversion of the experimental measurements of the heat capacity $C_v(E)$ and the static loading locus $E_s(V)$ into the complete EOS for hydrocode $S(V, E)$ is fulfilled with the help of other operators, as compared with equations 9 or 10. The operators remain integral in the case of nonconstant heat capacity. For the case of constant heat capacity, the operator becomes functional but transcendental. Singularities in this case appear when the ambient absolute temperature is equal to 0 K as many reserchers prefer. Of course, the assumption of constant heat capacity does not work in the vicinity of 0 K.

For explicit formulas for other types of experimental data, see Grinfeld (11).

2.2 Verification of Equations 1 and 2 for the EOS (5)

Combining equation 3 with the thermodynamic identities

$$\frac{\partial S(E, V)}{\partial E} = \frac{1}{T}, \quad \frac{\partial S(E, V)}{\partial V} = \frac{P}{T}, \quad (13)$$

we get

$$\frac{P}{T} = R \frac{\Delta(V)}{V}, \quad T = A + \int_{E_*}^E \frac{d\eta}{\chi(\eta)}. \quad (14)$$

Thus, the absolute temperature for the model under discussion depends upon the internal energy only, and constant A has the physical meaning of the absolute temperature at $E = E^*$.

Equation 14 proves equation 2. Combining equation 14 with the thermodynamic identity

$$C_v = \left(\frac{\partial T(V, E)}{\partial E} \right)^{-1}, \quad (15)$$

we arrive at equation 2:

$$C_v = \chi(E) = C_v(E). \quad (16)$$

3. Discussion and Conclusion

We suggest a novel class of simple EOS for hydrocode, depending on two functions of one variable each. The suggested $\Delta\chi$ – models generalize some classical models but also allow a wider set of degrees of freedom. Functions $\Delta(V)$ and $\chi(T)$ should be recovered by comparing available experimental data.

This is not the most general form of the complete EOS. Some data, when available, cannot be considered in the suggested framework. A much more general class of the EOS is suggested in a future report (11). On the other hand, the suggested model has its own advantages. First, it allows further analytical consideration. Second, it can be recommended in cases where the scope of data is relatively narrow.

We established the explicit formulas for the recovery of the complete EOS for hydrocode from experimental data for the heat capacity at constant volume C_V and the loci of the Hugoniot or static adiabata. The recovery formulas have the form of integral operators with certain singularities. Those formulas can be relatively easily implemented into computer code. Vigilance is necessary in handling the singularities.

The suggested EOS is complete in the sense that it automatically satisfies the First and Second Laws of Thermodynamics.

4. References

1. Bridgman, P. W. *The Nature of Thermodynamics*; Harvard University Press: Cambridge, MA, 1941.
2. Bridgman, P. W. *The Physics of High Pressure*; Bell and Sons, 1931.
3. Grinfeld, M. A. *Thermodynamic Methods in the Theory of Heterogeneous Systems*; Longman: New York, 1991.
4. MacDonald, J. R. Review of Some Experimental and Analytical Equations of State. *Rev. Mod. Phys* **1969**, *41*, 316–349.
5. Zharkov, V. N.; Kalinin, V. A. *Equations of State for Solids at High Pressures and Temperatures*; Consultants Bureau, 1971.
6. Anderson, O. L. *Equations of State of Solids for Geophysics and Ceramic Science*; Oxford University Press: New York, 1995.
7. Eliezer, S.; Ghatak, A.; Hora, H. *Fundamentals of Equations of State*; World Scientific: Singapore, 2002.
8. Menikoff, R. Empirical EOS for Solids. In *Shock Wave Science and Technology Reference Library*, 2, *Solids I*; Horie, I., Ed.; Springer: New York, 2007.
9. Zel'dovich, Ya.; Raizer, B.; Yu. P. *Physics of Shock Waves and High-Temperature Hydrodynamic Phenomena*; Dover, 2002.
10. Landau, L. D.; Lifshits, E. M. *Fluid Mechanics*; Pergamon Press: Elmsford, NY, 1989.
11. Grinfeld, M. A. The $\alpha\rho\lambda$ – Equation of State. U.S. Army Research Laboratory: Aberdeen Proving Ground, MD, to be published.

NO. OF
COPIES ORGANIZATION

1 (PDF only)	DEFENSE TECHNICAL INFORMATION CTR DTIC OCA 8725 JOHN J KINGMAN RD STE 0944 FORT BELVOIR VA 22060-6218
1	DIRECTOR US ARMY RESEARCH LAB IMNE ALC HRR 2800 POWDER MILL RD ADELPHI MD 20783-1197
1	DIRECTOR US ARMY RESEARCH LAB RDRL CIO LL 2800 POWDER MILL RD ADELPHI MD 20783-1197
1	DIRECTOR US ARMY RESEARCH LAB RDRL CIO MT 2800 POWDER MILL RD ADELPHI MD 20783-1197
1	DIRECTOR US ARMY RESEARCH LAB RDRL D 2800 POWDER MILL RD ADELPHI MD 20783-1197

NO. OF
COPIES ORGANIZATION

1	LOS ALAMOS NATIONAL LAB J BOETTGER MS F699 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB S CROCKETT MS B221 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB M T GREENFIELD MS P915 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB S R GREENFIELD MS J565 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB R MENIKOFF MS B214 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB B J JENSEN MS B952 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB J N JOHNSON LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB B PLOHR MS B213 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB L SMILOWITZ MS P915 LOS ALAMOS NM 87545
1	LOS ALAMOS NATIONAL LAB D PRESTON LOS ALAMOS NM 87545
1	SANDIA NATIONAL LABS J H CARPENTER MS 1322 ALBUQUERQUE NM 87185
2	SANDIA NATIONAL LABS M DESJARLAIS MS 1189 T R MATTSON MS 1189 ALBUQUERQUE NM 87185
1	SANDIA NATIONAL LABS R J MAGYAR MS 1322 ALBUQUERQUE NM 87185

NO. OF
COPIES ORGANIZATION

1	SANDIA NATIONAL LABS S SCHUMACHER MS 0836 ALBUQUERQUE NM 87185
1	SANDIA NATIONAL LABS E STRACK MS 0378 ALBUQUERQUE NM 87185
1	SANDIA NATIONAL LABS T VOGLER LIVERMORE CA 94550
3	LAWRENCE LIVERMORE NATL LABS L BENEDICT M A BARRIOS A TEWELDEBERHAN 7000 EAST AVE LIVERMORE CA 94550
1	NAVAL SURFACE WARFARE CTR RESEARCH AND TECHLGY DEPT G T SUTHERLAND INDIAN HEAD MD 20640
1	APPLIED RESEARCH ASSOC D GRADY 4300 SAN MATEO BLVD A-220 ALBUQUERQUE NM 87110
1	US AIR FORCE RESEARCH LAB MUNITIONS DIRCTRT Y HORIE EGLIN AFB FL 32542
2	THE JOHNS HOPKINS UNIV DEPT OF MECH ENGRG K T RAMESH T W WRIGHT 232 LATROBE HALL 3400 N CHARLES ST BALTIMORE MD 21218
2	UNIVERSITY AT STONY BROOK J GLIMM R SAMULYAK STONY BROOK NY 11794-3600
2	UNIVERSITY OF SOUTH FLORIDA DEPT OF PHYSICS I OLEINIK V ZHAKHOVSKY TAMPA FL 33620

NO. OF
COPIES ORGANIZATION

1 UNIV OF UTAH
DEPT OF MECH ENGRG
R BRANNON
50 S CENTRAL CAMPUS DR
SALT LAKE CITY UT 84112

1 UNIV OF CALIFORNIA
DEPT OF MECH & ARSPC ENGRG
V NESTERENKO
9500 GILMAN DR
LA JOLLA CA 92093-0411

1 UNIV OF MD
DEPT OF MECHANICAL ENGRG
R ARMSTRONG
COLLEGE PARK MD 20742

1 UNIV OF COLORADO AT BOULDER
DEPT OF CIVIL ENGRG &
ARCHITECTURAL ENGRG
R A REGUEIRO
428 UCB ECOT 441
1111 ENGRG DR
BOULDER CO 80309-0428

1 ROBERT R MCCORMICK SCHOOL
OF ENGRG & APPLIED SCI
H ESPINOSA
633 CLARK ST
EVANSTON IL 60208

1 UNIV OF MISSOURI
DEPT OF CHEMISTRY
T SEWELL
COLUMBIA MO 65211-7600

1 UNIV OF MD
DEPT OF MATERIALS SCI & ENGRG
M KUKLJA
COLLEGE PARK MD 20742

1 STANFORD UNIV
DEPT OF AERONAUTICS &
ASTRONAUTICS
R CHRISTENSEN
DURAND BLDG 496
LOMITA MALL
STANFORD CA 947305-4035

1 US ARMY RESEARCH OFFICE
RDRL RO
D SCUTRUD
BLDG 4300
DURHAM NC 27703

NO. OF
COPIES ORGANIZATION

1 US ARMY RESEARCH OFFICE
RDRL ROI
B WEST
BLDG 4300
DURHAM NC 27703

1 US ARMY RESEARCH OFFICE
RDRL ROI M
J MYERS
BLDG 4300
DURHAM NC 27703

2 US ARMY RESEARCH OFFICE
RDRL ROE M
J PRATER
D STEPP
BLDG 4300
DURHAM NC 27703

1 US ARMY RESEARCH OFFICE
RDRL ROE N
R ANTHINIEN
BLDG 4300
DURHAM NC 27703

3 US ARMY RESEARCH OFFICE
J LAVERY
D MANN
S MATHAUDHU
BLDG 4300
DURHAM NC 27703

ABERDEEN PROVING GROUND

72 DIR USARL
RDRL WM
B FORCH
J MCCAULEY
S KARNA
P PLOSTINS
RDRL WMP B
R BECKER
S BILYK
D CASEM
J CLAYTON
D DANDEKAR
J FITZPATRICK
M GRINFELD (20 CPS)
C HOPPEL
R KRAFT
B LEAVY
D POWELL
M RAFTENBERG
M SCHEIDLER

NO. OF
COPIES ORGANIZATION

T WEERASOORIYA
C WILLIAMS
RDRL WMP C
T BJERKE
S SEGLETES
W WALTERS
RDRL WML B
I BATYREV
J BRENNAN
S IZVEKOV
B RICE
RDRL CIH C
P CHUNG
J CAZAMIAS
J KNAP
RDRL WMM G
I ANDZELM
F BEYER
J LENHART
B RIDERSPACHER
RDRL WMP E
W GOOCH
B LOVE
C KRAUTHAUSER
RDRL WMM E
J ADAMS
L KECSKES
J LASALVIA
P PATEL
J SWAB
M WILL-COLE
RDRL WMM B
B CHEESEMAN
C FOUNTZOULAS
G GAZONAS
RDRL SER L
W NOTHWANG
RDRLWML H
M FERMEN-COKER
RDRL WMP
B BURNS
S SCHOENFELD
RDRL WMP D
H MEYER
RDRL WMP G
R BANTON
S KUKUCK

NO. OF
COPIES ORGANIZATION

- 1 CAVENDISH LAB
MOTT BLDG RM 316B
JJ THOMSON AVE
M CHAUDHRI
CAMBRIDGE CB3 0HE
UNITED KINGDOM
- 1 LOUGHBOROUGH UNIV
WOLFSON SCHOOL OF MECH &
MANUFACTURING ENGRG
LOUGHBOROUGH
V SILBERSCHMIDT
LE11 3TU
UNITED KINGDOM
- 1 UNIVERSITY OF LIVERPOOL
DEPT OF ENGRG
BROWNLOW HILL
LIVERPOOL
H OUYANG
L69 3GH
UNITED KINGDOM
- 4 AWE ALDERMARSTON READING
BERKSHIRE RG7 4PR
N BOURNE
J C F MILLETT
G A COX
C M ROBINSON
UNITED KINGDOM
- 1 DEFENCE SCI & TECHLGY
ORGANISATION
WEAPONS SYSTEMS DIV
A RESNYANSKY
EDINBURGH SA 5111
AUSTRALIA
- 1 CSIRO EXPLORATION & MINING
PO BOX 883
KENMORE QLD 4069
F D STACEY
AUSTRALIA
- 1 MOSCOW STATE UNIV
INSTITUTE OF MECHANICS
MICHURINSKIE PR 1
S S GRIGORYAN
MOSCOW 117192
RUSSIA

NO. OF
COPIES ORGANIZATION

- 1 STEKLOV MATHEMATICAL
INSTITUTE
GUBKINA AV 8
A G KULIKOVSKII
MOSCOW 117966
RUSSIA
- 1 LANDAU INSTITUTE FOR
THEORETICAL PHYSICS
N INOGAMOV
RAS CHERNOGOLOVKA 142432
RUSSIA
- 5 JOINT INSTITUTE FOR HIGH
TEMPERATURE PHYSICS
RUSSIAN ACADEMY OF SCIENCES
V FORTOV
V GRYAZNOV
G KANEL
M LOMONOSOV
S RAZORENOV
JIHT RAS MOSCOW 125412
RUSSIA
- 1 INSTITUTE OF CONTINUOUS MEDIA
MECHANICS
URAL BRANCH OF RAS
O B NAIMARK
1 ACAD KOROLEV STR
PERM 614013
RUSSIA
- 1 BEN GURION UNIV
DEPT OF MECHANICAL ENGRG
E B ZARETSKY
PO BOX 653
BEER SHEVA 84105
ISRAEL
- 1 RAFAEL
PO BOX 2250
Y PARTOM
HAIFA 31021
ISRAEL